

Trigonometry

csc θ = 1/ sin θ  
sec θ = 1/ cos θ  
sin(π/2 - θ) = cos θ  
cos(π/2 - θ) = sin θ  
cos(2θ) = cos<sup>2</sup> θ - sin<sup>2</sup> θ  
cos(2θ) = 2 cos<sup>2</sup> θ - 1  
cos(2θ) = 1 - 2 sin<sup>2</sup> θ  
tan(2θ) = 2 tan θ / (1 - tan<sup>2</sup> θ)  
sin θ + sin φ = 2 sin((θ + φ)/2) cos((θ - φ)/2)  
sin θ - sin φ = 2 cos((θ + φ)/2) sin((θ - φ)/2)  
cos θ + cos φ = 2 cos((θ + φ)/2) cos((θ - φ)/2)  
cos θ - cos φ = -2 sin((θ + φ)/2) sin((θ - φ)/2)  
sin θ sin φ = (cos(θ - φ) - cos(θ + φ))/2  
cos θ cos φ = (cos(θ - φ) + cos(θ + φ))/2  
sin θ cos φ = (sin(θ + φ) + sin(θ - φ))/2  
cos θ sin φ = (sin(θ + φ) - sin(θ - φ))/2  
sinh x = (e<sup>x</sup> - e<sup>-x</sup>)/2  
cosh x = (e<sup>x</sup> + e<sup>-x</sup>)/2

Models

Newton's Law of Cooling

dT/dt = -k(T - T\_m), T(t\_0) = T\_0  
where T(t) is temperature of body at time t, k > 0 is coefficient of heat transfer (constant) and T\_m is temperature of surroundings (assumed to be an infinite reservoir that can absorb any amount of heat without changing its temperature).

T(t) = T\_m + (T\_0 - T\_m)e^{-k(t-t\_0)}

Draining a Tank

Rate of volume of liquid leaving the tank is proportional to, A\_h v, where A\_h is area of hole, dV/dt = -A\_h sqrt(2gh)  
Finally, volume of liquid in tank is V(t) = A\_w h, where A\_w is (constant) area of tank dh/dt = -A\_h/A\_w sqrt(2gh), h(t\_0) = h\_0

h(t) = (h\_0^{1/2} - (A\_h sqrt(2g) / (2 A\_w)) (t - t\_0))^2

Population Growth

dP/dt = rP, P(t\_0) = P\_0 (one parameter model: r)  
where P(t) is the population at time t and r is the rate of population growth. Linear equation can be solved easily by integration. Gives (disastrous!) exponential population growth:  
int\_{P\_0}^P dP/P = int\_{t\_0}^t r dt => log(P(t)/P\_0) = r(t - t\_0)  
P(t) = P\_0 e^{r(t-t\_0)}

Realistic Population Growth

dP/dt = rP(1 - P/K) (two parameter model: r, K)  
where r is rate of population growth and K is the carrying capacity (the long time stable equilibrium population). This is also an autonomous ODE.

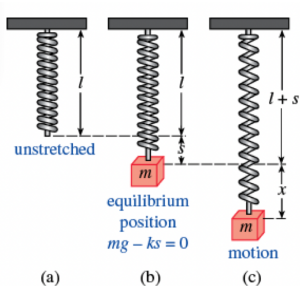
P(t) = P\_0 K / (P\_0 + (K - P\_0)e^{-rt})

Beam deflection

TABLE 3.9.1.

Ends of the Beam	Boundary Conditions
Embedded	y = 0, y' = 0
Free	y'' = 0, y''' = 0
Simply supported or hinged	y = 0, y'' = 0

Hook's Law of Springs



Spring motion when deformed by gravity F\_g = -mg, where m is mass of suspended weight. s > 0 is equilibrium displacement under gravity (i.e. gravitation force balances restoring spring force). x is additional displacement from equilibrium position (spring is stretched or compressed).

- Hooke's law: F\_s = -k(s + x). (additional elongation x compared to equilibrium elongation s under gravity) Note: x > 0 indicates downward displacement ("Reversed coordinates")
- Force exerted on mass m by gravity: F\_g = mg. (Positive sign due to reversed coordinates!)
- Newton's second law: F = ma = m x''

Force balance: m x'' = F\_s + F\_g => m x'' = -k(s + x) + mg => -kx + (mg - ks) = 0  
=> x'' + (k/m)x = 0  
=> x'' + omega^2 x = 0  
where omega = sqrt(k/m) is natural frequency of oscillations.

x(t) = c\_1 cos omega t + c\_2 sin omega t  
Simple harmonic motion with angular frequency omega, period T = 2pi/omega and frequency 1/T = omega/(2pi). Simple harmonic motion is also known as free vibration because dynamical system is homogeneous (unforced, apart from gravity).

Equation of motion for simple harmonic motion  
x(t) = c\_1 cos omega t + c\_2 sin omega t  
Is often written in an equivalent form involving two different constants: the amplitude A and phase phi  
x(t) = A cos(omega t - phi)  
where A = sqrt(c\_1^2 + c\_2^2) and phi = arctan(c\_1/c\_2).

Dampened spring system

m x'' = -kx - beta x'

where beta > 0 is damping constant.

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x'' + 2 lambda x' + omega^2 x = 0  
where 2 lambda = beta/m and omega^2 = k/m  
Auxiliary equation is: r^2 + 2 lambda r + omega^2 = 0 with solutions r = - lambda +/- sqrt(lambda^2 - omega^2).  
3 Cases:  
1. Overdamped: lambda^2 - omega^2 > 0 (distinct real roots: exponential decay of motion as t -> infinity).  
2. Critically damped: lambda^2 - omega^2 = 0 (repeated real root: any slight decrease in damping -> oscillations).  
3. Underdamped: lambda^2 - omega^2 < 0 (complex conjugate roots: oscillations with decreasing amplitude).  
Can also apply external forcing:  
Suppose we apply external force f(t) to suspended mass (e.g. push or pull it).  
Dynamical system is now nonhomogeneous:  
m x'' + beta x' + kx = f(t)  
or, dividing by m,  
x'' + 2 lambda x' + omega^2 x = F(t)  
where F(t) = f(t)/m.

L[y] = y'' + P(x)y' + Q(x)y = f(x)

Thus, given complementary function y\_c = c\_1 y\_1 + c\_2 y\_2, particular solution is  
y\_p = u\_1 y\_1 + u\_2 y\_2  
where  
u\_1(x) = int (W\_1(x)/W(x)) dx = - int (y\_2(x)f(x)/W(x)) dx, u\_2 = int (W\_2(x)/W(x)) dx = int (y\_1(x)f(x)/W(x)) dx

Cauchy Euler Equations

General solution is y = x^m:

L[y] = ax^2 d^2y/dx^2 + bx dy/dx + cy = g(x)

Auxiliary equation: am^2 + (b - a)m + c = 0

Case 1: distinct real roots m\_1, m\_2 in R

y\_c(x) = c\_1 x^{m\_1} + c\_2 x^{m\_2}

Case 2: repeated root m in R

y\_c(x) = c\_1 x^m + c\_2 x^m log x

Case 3: complex conjugate roots alpha +/- i beta, alpha, beta in R

y\_c(x) = x^alpha [c\_1 cos(beta log x) + c\_2 sin(beta log x)]

Partial differential equations

variations  
Consider PDE with constant coefficients A, B, C, D, E, F:  
A d^2u/dx^2 + B d^2u/dxdy + C d^2u/dy^2 + D du/dx + E du/dy + F u = G(x, y)  
We classify PDE as one of three types according to value of B^2 - 4AC

B^2 - 4AC { > 0 hyperbolic (e.g. wave equation),  
= 0 parabolic (e.g. heat equation),  
< 0 elliptic (e.g. Poisson equation).

For example, if there is heat transfer from the lateral surface of a rod into a surrounding medium that is held at a constant temperature u\_m, then the heat equation (13) is

k d^2u/dx^2 - h(u - u\_m) = du/dt,

where h is a constant. In (14) the function F could represent the various forces acting on the string. For example, when external, damping, and elastic restoring forces are taken into account, (14) assumes the form

external force, damping, restoring force  
a^2 d^2u/dx^2 + f(x, t) - c du/dt - ku = d^2u/dt^2. (15)  
F(x, t, u, u\_t)

heat equation

k d^2u/dx^2 = du/dt

wave equation

a^2 d^2u/dx^2 = d^2u/dt^2

laplace equation

d^2u/dx^2 + d^2u/dy^2 = rho(x, y)

We found general solution  
Y(y) = c\_3 cosh(npi y/a) + c\_4 sinh(npi y/a)  
Imposing BC Y(0) = 0 => c\_3 = 0 => eigenfunction solutions compatible with BC are  
Y\_0(y) = y, n = 0, Y\_n(y) = sinh(npi y/a), n = 1, 2, 3, ...  
Finally, using u\_n(x, y) = X\_n(x) Y\_n(y) we find the complete set of eigenfunctions  
u\_0(x, y) = y, n = 0 and u\_n(x, y) = A\_n cos(npi x/a) sinh(npi y/a), n = 1, 2, 3, ...

Linear combinations of eigenfunctions give general solution

u(x, y) = A\_0 y + sum\_{n=1}^infinity A\_n cos(npi x/a) sinh(npi y/a)

How do we impose BC u(x, b) = f(x)?

By computing coefficients A\_n such that

u(x, b) = f(x) = A\_0 b + sum\_{n=1}^infinity (A\_n sinh(npi b/a)) cos(npi x/a)

Need to compute coefficients A\_n from Fourier series for f(x) by setting y = b:  
u(x, b) = f(x) = A\_0 b + sum\_{n=1}^infinity (A\_n sinh(npi b/a)) cos(npi x/a)  
A\_0 b = 1/2 a int\_0^a f(x) dx => A\_0 = 1/(ab) int\_0^a f(x) dx Note extra factor 1/2 for A\_0, cosine series coefficient!  
A\_n sinh(npi b/a) = 2/a int\_0^a f(x) cos(npi x/a) dx => A\_n = (2/(a sinh(npi b/a))) int\_0^a f(x) cos(npi x/a) dx, n = 1, 2, 3, ...

$f(x) = A_0 b + \sum_{n=1}^{\infty} \left( A_n \sinh \frac{n\pi b}{a} \right) \cos \frac{n\pi x}{a},$  where coefficients  $A_n$  are given by

$A_0 = \frac{1}{ab} \int_0^a f(x) dx, \quad A_n = \frac{2}{a \sinh \frac{n\pi b}{a}} \int_0^a f(x) \cos \frac{n\pi x}{a} dx, \quad n = 1, 2, 3, \dots$